

: 531.3.631.544.63

õ

ö

5 310202 ó

:

• • •

ó 2016

	3
I-	.		-
		10
1.1.			
	,	10
1.2.			
		23
1.3.		34
II-	.		
		39
2.1.			
		39
2.2.			
		41
2.3.			
		57
		57
III-	.		
		70
3.1.			
		70
3.2.			
	í	74
3.3.			
		77
3.4.			
		85
	í í	89
		92

ó

,

,

• •

.

,

,

[1].

-

.

,

()

.

õ

ö

,

,

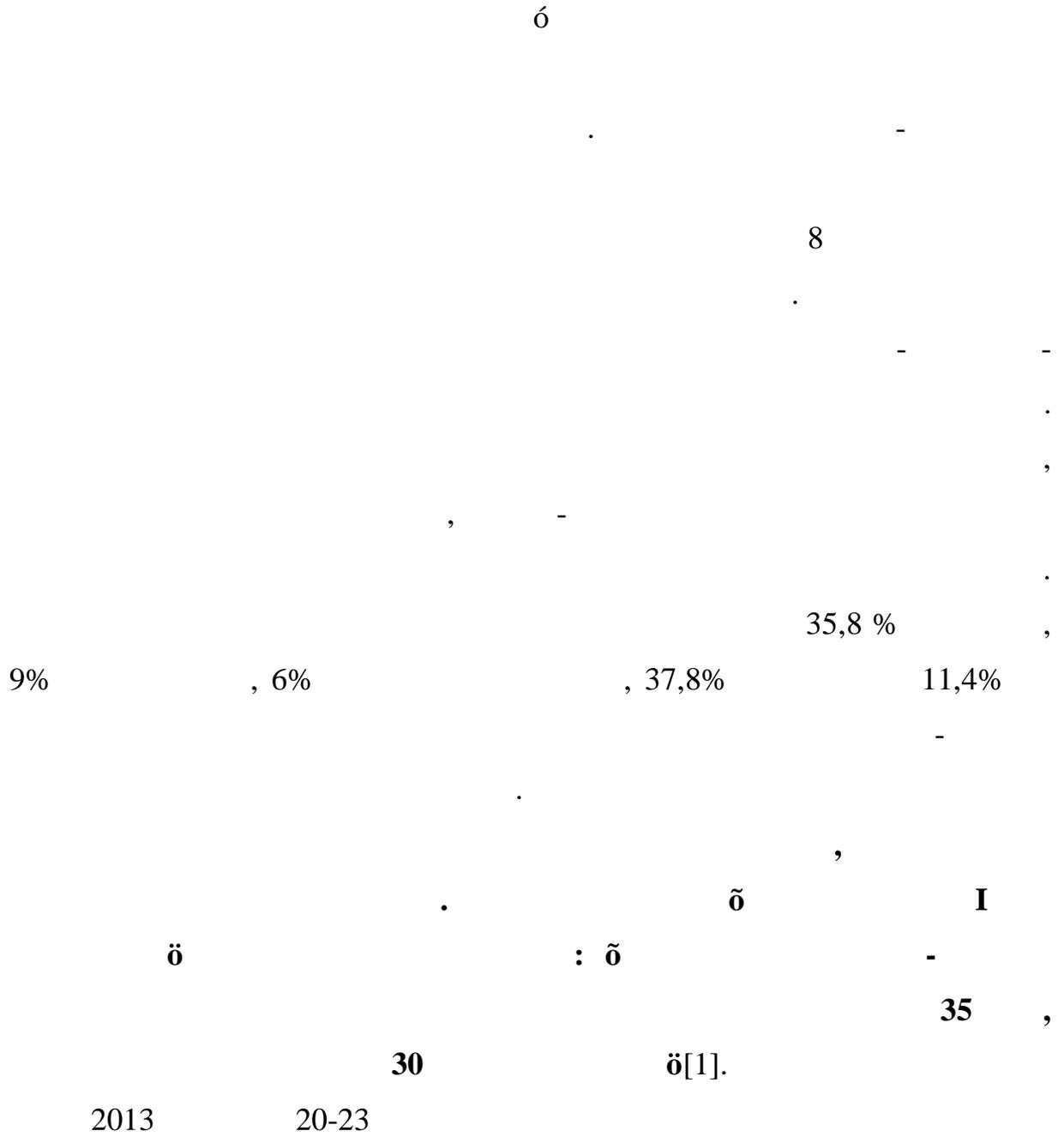
-

.

ó

.

[2].



2013

20-23

30

ö[1].

2030

2

105

-

,

. 2013 1
-4512- ð

-

ö

.

,

100

,

.

, - ð ö (,
...)

...

2013 1 ð

- ö 4512-

.

,

-

.

-

.

, ,

,

, ,

-

.

,
 .
 ,
 2410-3200 ,
 12 , 5-6
 .
 () 1500÷2000
 , 0,15
 [3].
 ,
 .
 : , , , ,
 1
 / ² . - 1 ² 8-10
 ,
 1,23-1.26 ()
 . -
 300063200 ,
 .
 .
 .
 (,)
 -
 .

, 1

5

10

50%

·
· ð 30 ·
ö (-4-47)

-

·

·

-

-

·

:

:

-

2

;

-

-

;

-

-

;

-

·

I- .

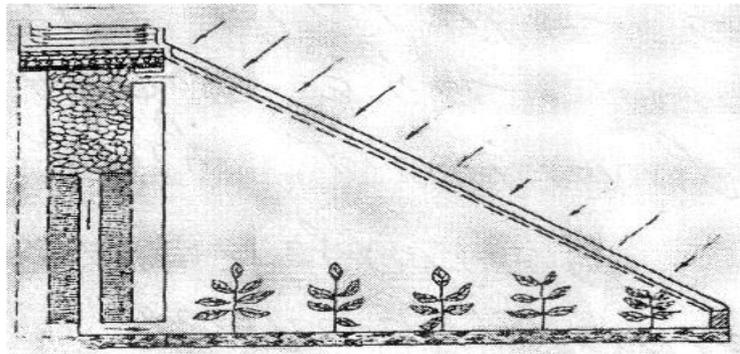
1.1.

,

1960-1970-

1.1-

. [5]



1.1-

$$65 = 240^2$$
$$3,7 \quad 7 = 26^2$$

$$0,3 \quad 1 \quad 3,7 \quad 6,5$$

0,25 1 2

1

[5]

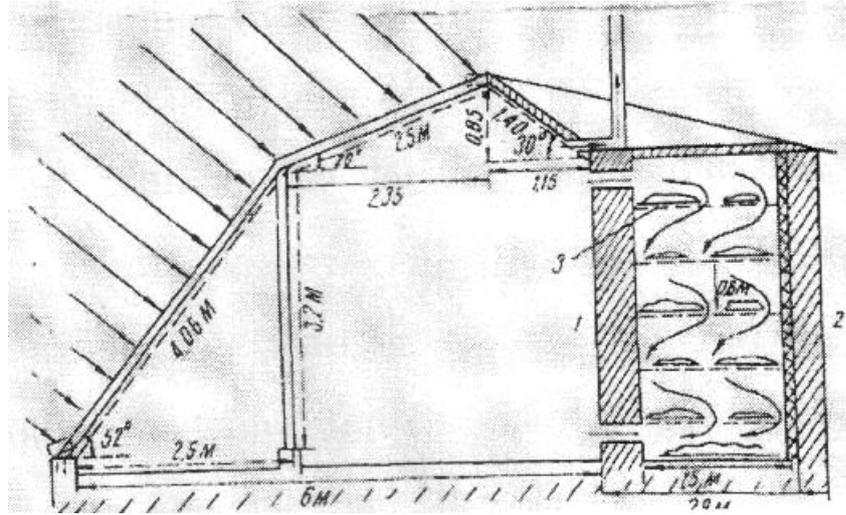
1.2-

$$V = F \cdot h \cdot n = 13m^2 \cdot 0,25m \cdot 5 = 17m^3 \quad (1.1)$$

; n-

õ ö

[6]



1.2-

1971-

45°

100²

. [6]

$$l = 10,0 \text{ ,}$$

$$h = 5,0 \text{ ,}$$

$$\alpha_x = 45^0 \text{ ,}$$

$$\alpha = 20^0 \text{ .}$$

$$l = 11,0 \text{ ,}$$

$$h = 5,0$$

$$\alpha = 45^0 \text{ , } \alpha = 20^0 \text{ .}$$

$$0,25$$

$$\frac{1}{0,40}$$

$$15$$

$$1^2$$

$$0,18^3$$

$$0,15^3$$

$$1000^2$$

. [7]

ó

770 / ², 1

1000

3

.

150

3

.

1965-1970-

.

.

.

.

: ,

,

.

.

,

2⁰- 3⁰

.

:

-

,

.

8⁰-10⁰

,

7⁰-10⁰

.

,

.

:

.

,

.

:

1977-1978

25 6=150²

-0.7

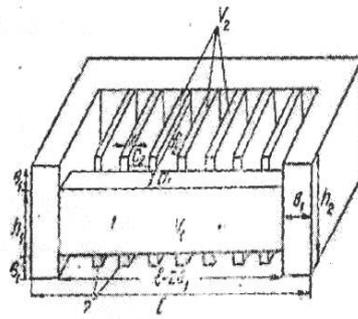
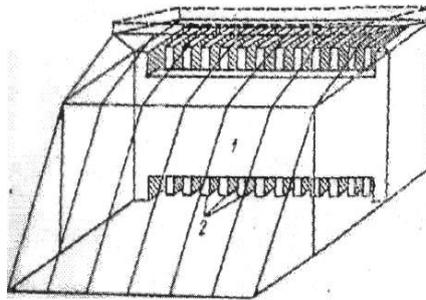
ö

ö

6, 9, 12, 15, 18, 21, 24, 27

30

[8]



1.3-

tw,tx/2

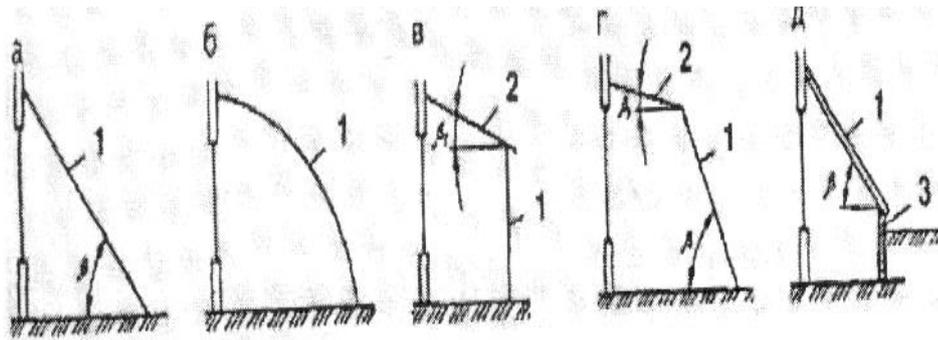
t_f

t_n,

t_{yu},

()

1.4-



1.4-

;)
 ;)
 ;)
 ;)
 ;)
 ; 1- ; 2-
 ; 3- ;

50.....60⁰

20.....35⁰

1:1,5

. [9]

1985-1990-

50² (

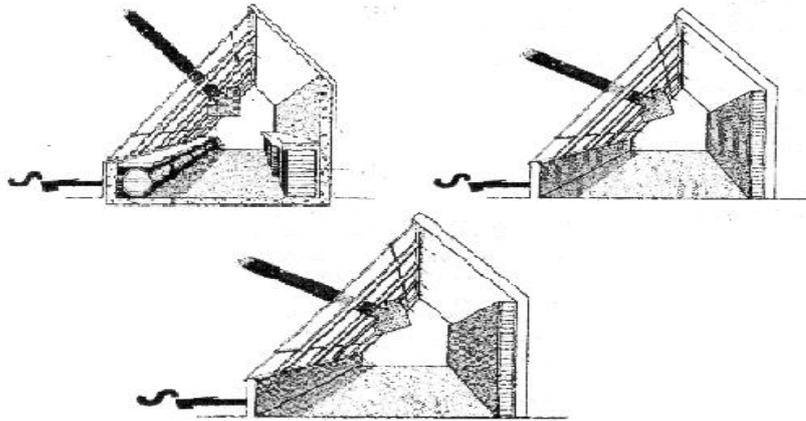
10 , 5) .

0,6 ,

0,5

.
 : (1.5-)
 1,5-1,8
 ,
 d=25
 50 25

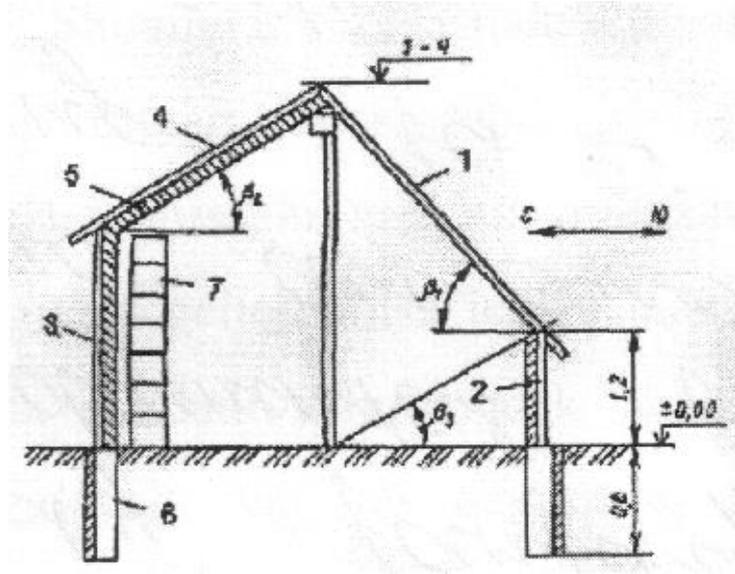
[10]



1.5-

ó

(, -) .



1.6-

- 1- ; 2- ; 3-
 ; 4-
 ; 5- ; 6-
 ; 7- ;

1-

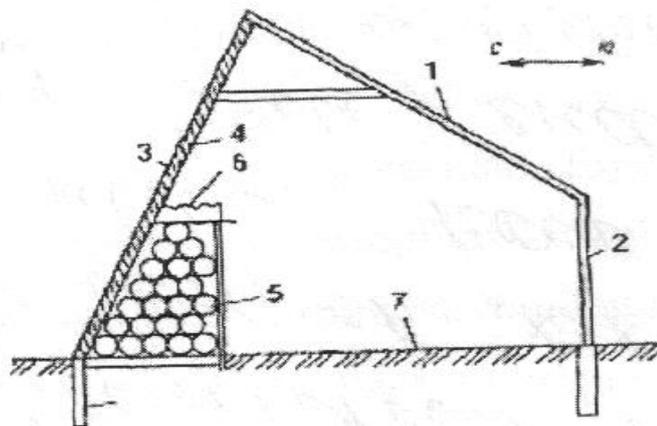
β_1

, 2-

β_2

()

1.7-



1.7-

1-

; 2-

; 3-

; 4-

; 5-

; 6-

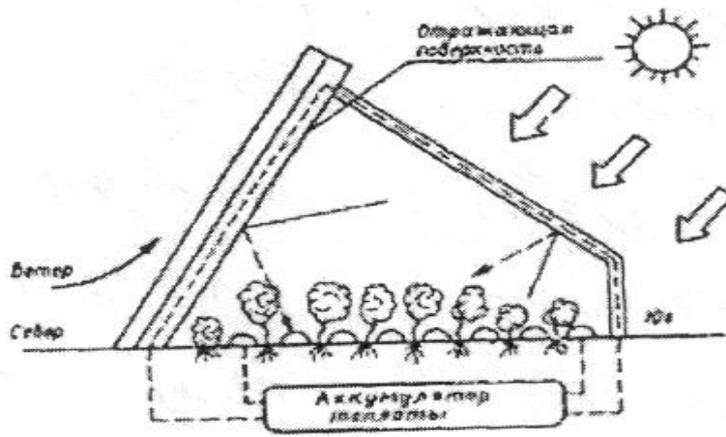
8- ; 7- ;

1...1,5
20...35

1²

50-70

1.8-



1.8-

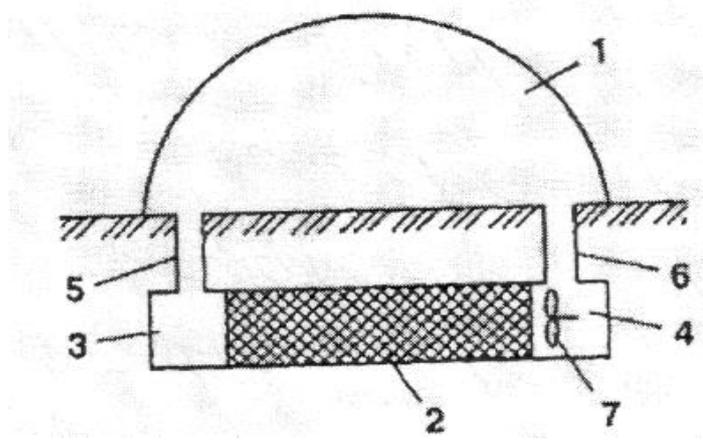
5-6

v -

38-40⁰

25-30⁰

(10-12⁰)



1.9-

1.2.

. [11]

) (.

1.1.-

(95%)

(0,29.....2,4 μ)

5		0,62.....0,76
6		0,76..... 3×10^3
7		76.....2,3
		3×10^3

1.2-

/		$\lambda^m, \mu km$
1	()	0,3.....4
1.1	()	0,38.....0,71
1.2	()	0,35.....0,75
	-	0,4
	-	0,4..... 0,5
	-	0,5.....0,6
	-	0,6..... 0,7
1.3		0,7
2		0,75..... 4
		4

,

,

J_{\perp}

1,368....1,377 / ²

1,331...1,428 / ²

$J_0 = 1,37$ / ²

. [11]

,

$$I_2 = I_0 \sinh \quad (1.2)$$

$$\sinh = \sin \varphi \cdot \sin \delta + \cos \varphi \cdot \cos \delta \cdot \cos \tau^0 \quad (1.3)$$

$$\tau^0 = \omega \tau; \quad \omega = 2\pi/T; \quad = 24 \quad (1.4)$$

$\tau -$ ()

$$Q_{or} = \int_{-\tau_0}^{+\tau_0} I_{or} d\tau \quad (1.5)$$

$+\tau_0, -\tau_0-$

$\sinh = 0$

(1.2), (1.5)

, Q_{or}

φ

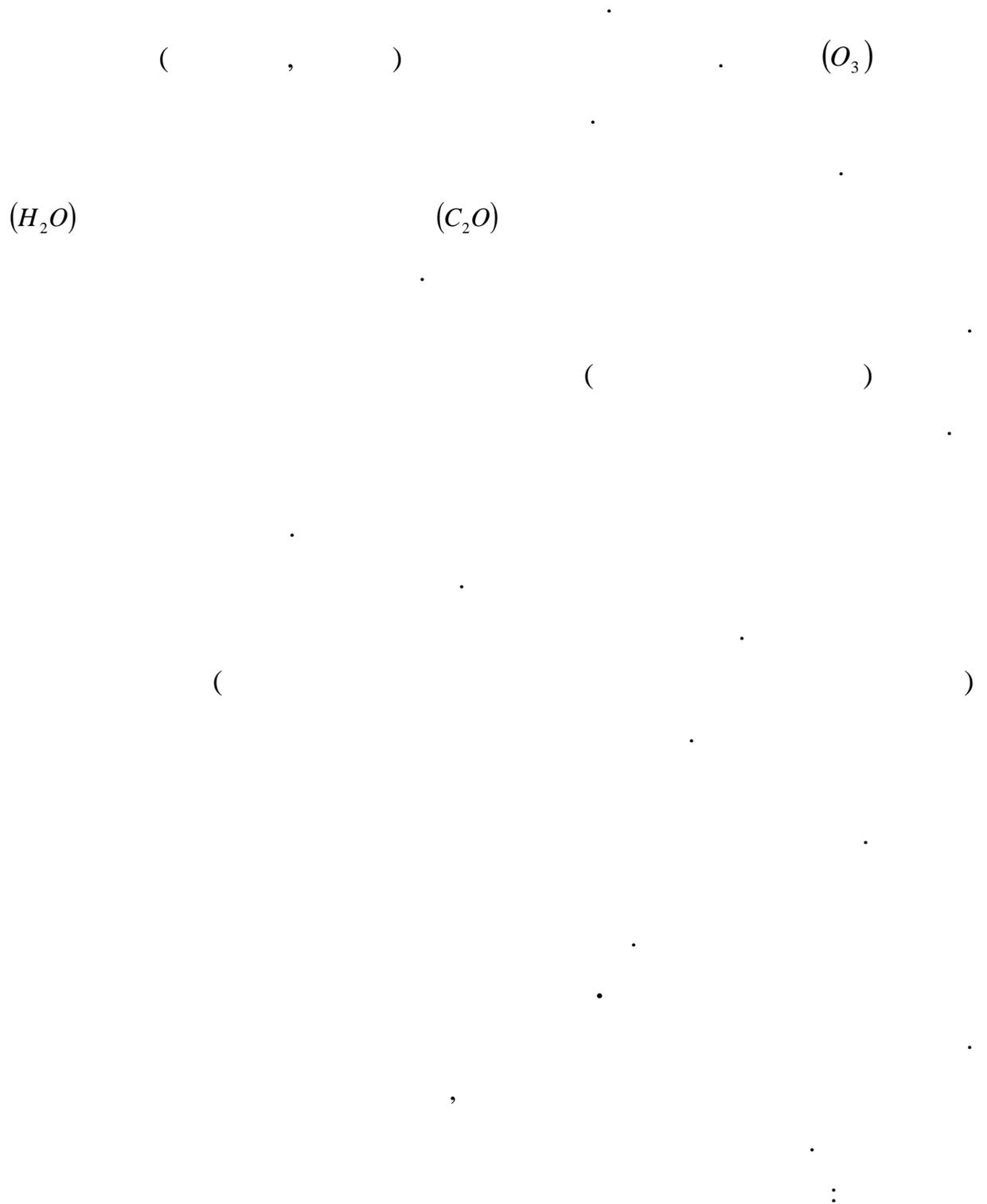
δ ()

, Q_{or}

$$Q_{or} = \frac{T3600}{\pi} I_0 K_0 \cos \varphi \cdot \cos \delta (\sin \tau - \tau \cos \tau) \quad (1.6)$$

$$K_0 = 110,0335 \cos \left(\frac{360N}{365} \right); \quad \delta = (23,45^0) \sin \gamma \quad (1.7)$$

$$\gamma = \frac{360(284 + N)}{365,24}; \quad \tau = \arccos(-\operatorname{tg} \varphi \cdot \operatorname{tg} \delta) \quad (1.8)$$



$$S_2 = S_{\perp} \sinh \quad (1.9)$$

$$S_K = S_{\perp} \cos i; \quad (1.10)$$

$$\cos i = \cos i \sinh + \sin \alpha \cosh \cos \psi ;$$

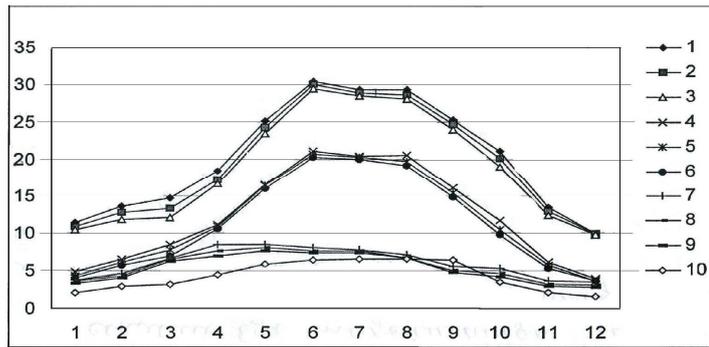
$$\psi = \psi_0 + \psi_k ; \quad (1.11)$$

$$\cos \psi_0 = \frac{\sinh \cdot \sin \varphi - \sin \delta}{\cosh \cdot \cos \varphi}; \quad \sin \psi_0 = \frac{\sin \tau^0 \cdot \cos \delta}{\cosh} \quad (1.12)$$

ψ_0

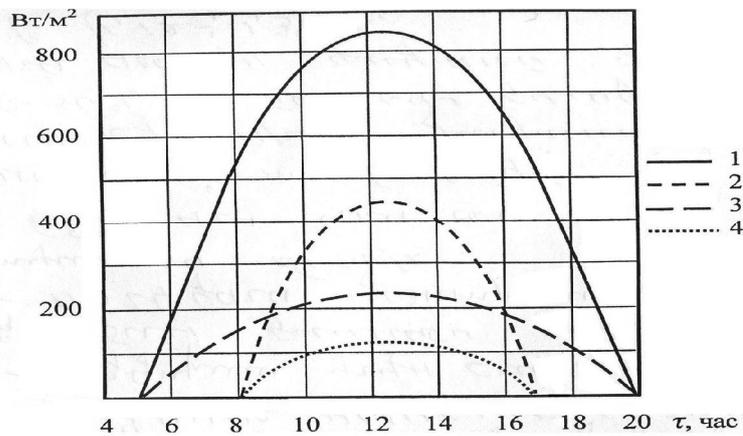
ψ_k

$(\varphi = 39^\circ)$



1.10-

(τ^2), ; 1- S_{\perp} - ; 2- S_{\perp} - ; 3- S_{\perp} - ; 4- S - ; 5- S - ; 6- S - ; 7- D - ; 8- D - ; 9- D - ; 10- R - .



1.11-

$/^2$, ;

1- S_{\perp} -15/VI, 2- S_{\perp} -15/I, 3- D -15/VI, 4-15/I.

$$D_{\perp} = b(I_{\perp} - S_{\perp})\sinh; \quad D_2 = b(I_2 - S_2)\sinh. \quad (1.13)$$

$$b = 1/2, \quad b = 1/3$$

$$D_k = D_2 \cos^2(\alpha/2) \quad (1.14)$$

()

(30 %) (70 %),

$$R = Q/A \quad (1.15)$$

$$A = R/Q \quad (1.16)$$

$$Q = S + D + R ; \quad Q_{\perp} = S_{\perp} + D_{\perp} + R_{\perp} \quad (1.17)$$

$$Q_k = S_k + D \cos^2(\alpha/2) + R_2 \sin^2(\alpha/2) \quad (1.18)$$

[12]

1.

-

2.

-

3.

-

4.

-

5.

()

,

2

.

.

.

,

,

.

,

,

.

2

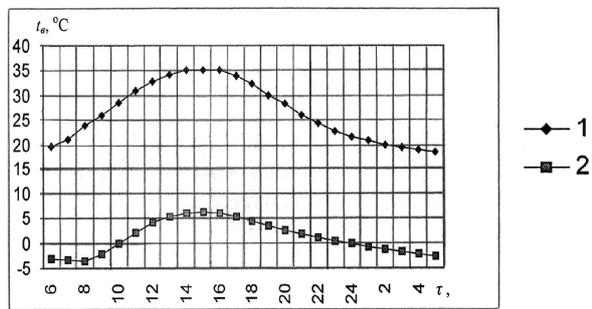
.

.

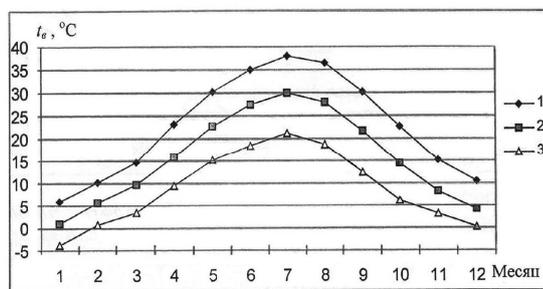
,

,

2....3



1.12-



1.13-

0

∴ 1-

; 2-

; 3-

.....

- 1. 2 ó
- 2. ó

.....
12 ó 15%

(37 45

2800-3100

1

5900-6300 (1650-1750 -)

200-215

·
, ,
, ,

99

· « »

XXI

·
,
,
·
·

· [14]

· ,
, ,
, ,
, ,
, ,
·

II- .

2.1.

$$= 273; \quad = 297 ; L = 1 \quad (\quad ^2 \cdot \quad); \quad h_x = 10^5 \quad ; F = 10 \quad ^2$$

. [15]

$$Q = \alpha (t_{xn} - t_x)F + \sum_j C_0 \varepsilon_{i-j} b_{i-j} \varphi_{i-j} + (1 - p_i)(E_i - J_i) + q \quad + q \quad / \alpha_x \quad (2.1)$$

(2.1)

$$q_k = \alpha_k (\tau_{xn} - \tau_x)$$

$$t_{xn} t_x -$$

$${}^0C; \alpha \text{ ó}$$

/ ²⁰

, 1 ²

9

$$t_{(n+1)\Delta Z, m\Delta x} = \frac{t_{n,\Delta Z} (m+1)\Delta X + tm\Delta\tau, (m-1)\Delta X}{2}$$

(2.2)

$n, \Delta Z -$

; -

1 Δ

2,

. $\Delta\tau$

$$\tau_{n,z+1} = (\tau_{n,z+1} + \tau_{n-1,z}) / 2$$

(2.3)

(2.2)

(2.3)

$\Delta\tau = \Delta\tau$

Q

:

$$Q = \frac{\lambda}{\Delta X} (t_{1,z+1} - t_{2,z}) \Delta \tau \quad (2.4)$$

$$\alpha t_{1,z+1} - \alpha t_x + \frac{\lambda}{\Delta X} t_{1,z+1} - \frac{\lambda}{\Delta X} t_{2,z} = 0 \quad (2.5)$$

, $t_{1,z+1}$,

$$\tau_{1,z+1} = \frac{\alpha t_x + \frac{\lambda}{\Delta X} t_{2,r}}{\alpha + \frac{\lambda}{\Delta X}} \quad (2.6)$$

$\Delta \tau < \Delta \tau$,

$(\Delta_0) \Delta \tau$,

$$\Delta X_0 = \sqrt{2\alpha \Delta Z} \quad (2.7)$$

Δ_3

(2.7)

Δ_1, Δ_2
n-

[16]

$$Q_1 = (t_{n-1,z} - t_{n,z}) \frac{\lambda_1}{\Delta x_1} \Delta \lambda \quad (2.8)$$

2.2.

:

:

- 1) - ;
- 2) - ;
- 3) () - ;
- 4) -

[17]

"

"

, 20²

40%

20²

30%

20²

15%

1²

0

$$Q_c = K Q . \quad (2.9)$$

$$K = \left(1 - \frac{D}{Q}\right) K_s + \frac{D}{Q} \frac{1 + \cos \alpha}{2} + A \frac{1 - \cos \alpha}{2} . \quad (2.10)$$

t_{xmin}	
$t_{xmin} \geq -10$	1,2
$-10 > t_{xmin} > -20 \text{ } ^\circ\text{C}$	1,1

$$Q = (t - t) \quad (2.15)$$

3

$$, \quad /(\text{ }^3 \text{ }).$$

$$= n \quad V / V; \quad (2.16)$$

$$= 1,25 \quad /(\text{ }^3 \text{ }).$$

$$(2.15) \quad (2.16)$$

$$Q = (+) V (t - t). \quad (2.17)$$

C
D

$$Q = K F D; \quad D = 24 \times 3600(t - t). \quad (2.18)$$

()

. 2.2 -

t

t

Q ,f

- () t

2.2-

	t ,
-	18
	20
	20
	16
	15
	18

(2.18)

. [18]

$$Q = G Q \quad (2.19)$$

$$= 0,5...0,6$$

(2.18) (2.19)

:

$$G = \frac{KF D}{Q \eta} \quad (2.20)$$

$$Q = 126CO + 108H_2 + 358CH_4 + 590C_2H_2 + 638C_2H_6 + 861C_3H_3. \quad (2.21)$$

(/ ³).

$$Q = 358CH_4 + 638C_2H_6 + 913C_3H_8 + 1187C_4H_{10} + 1461C_5H_{12} + 234H_2S ;$$

$$Q = 358 \times 88,3 + 638 \times 2,5 + 913 \times 0,6 + 1187 \times 0,7 + 1461 \times 3 + 234 \times 0,1 =$$

$$= 31611,4 + 1592,5 + 547,8 + 830,9 + 4383 + 23,4 = 38989 \quad / \text{ }^3.$$

$$= Q / 29300 = 38989 / 29300 = 1,33. \quad (2.22)$$

$$(16 \times 10 \times 3,5)^3$$

$$: V = (16 \times 10 \times 3,5)^3 = 560^3; V = 390^3;$$

$$F = (16+10) \times 2 \times 3,5 + (16+10)^2 = 342^2; t = 18^\circ\text{C}; t_x = 0^\circ\text{C} -$$

$$= 1,5 \quad / (\text{ }^2).$$

$$Q = 1,5 \times 342 \times 24 \times 3600 (18 - 0) = 7,978 \times 10^8 \quad / \text{c};$$

$$G = 7,978 \times 10^5 / (38989 \times 0,6) = 34,14^3 / ;$$

$$G = G = 34,14 \times 1,33 = 45,35 \quad . / .$$

$$Q \quad G, G \quad .$$

$$Q = Q K F \quad (2.23)$$

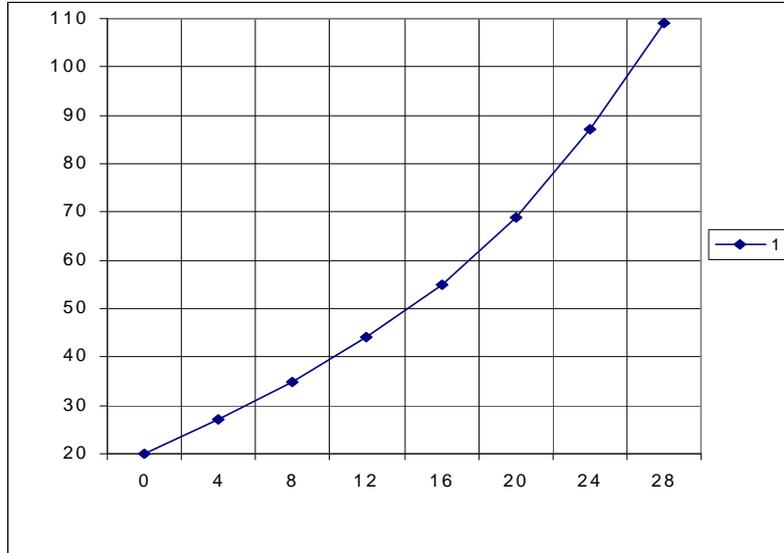
2.1-

f

$$f = Q / Q = 1 - Q / Q \quad (2.24)$$

f

$$q = Q_{<} F / Q \tag{2.25}$$



2.1-

: 1-f-

:

1)

f

;

2)

F

f

(,) $Q_{<} Q$, q
 f

Q

$$Q = (1 - f)Q$$

$f=0,4$

$$q = Q K F / Q = 1,65 \tag{2.26}$$

$$F = 1,65 \frac{Q}{Q K} \quad (2.27)$$

$$= \acute{e} 40$$

$$Q = 8,18 \quad / (\quad ^2 \quad), K = 1,7.$$

$$F = 1,65 \frac{7,978 \times 10^8}{8,18 \times 10^6 \times 1,7} = 94,7 \quad ^2 \acute{e} 95 \quad ^2 \quad (2.28)$$

$$= 0,4$$

$$Q = 8,18 \times 1,7 \times 95 \times 0,4 = 528,43 \quad /$$

:

$$V / F = 0,05 \quad ^3 / \quad ^2; \quad V = 0,05 \times 95 = 4,75 \quad ^3.$$

f

$$f_{max} = \frac{Q}{Q} 100\% = \frac{528,43}{797,8} 100\% = 66 \% \quad (2.29)$$

Q , *f*

2.3-

- 66%;

- 74%

4073

3

5394

Q, f

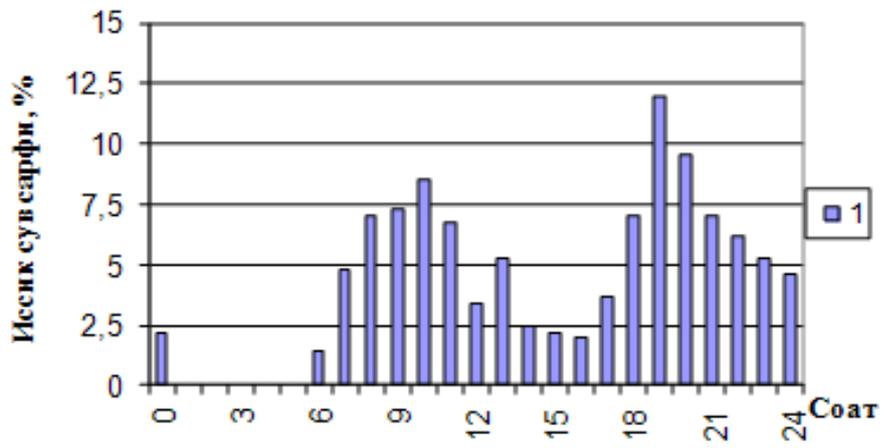
2.3-

	15/10	15/11	15/12	15/1	14/2	15/3	15/4
$Q, /(\text{ }^2)$	15,5	9,46	7,21	8,18	10,95	14,62	19,13
	1,34	1,62	1,8	1,7	1,43	1,19	1,01
$t_x, \text{ }^\circ\text{C}$	14	8	3	0	5	9	16
$Q, /$	177,3	443,2	664,8	797,8	576,2	398,9	88,65
G	1,45	$\frac{25,2}{456,1}$	$\frac{37,8}{1171}$	$\frac{45,35}{1406}$	$\frac{32,76}{917,2}$	$\frac{22,7}{680,3}$	$\frac{5,03}{150,8}$
$f_{max}, \%$	>>100	>100	74	66	>100	>100	>>100

50-70%

[19]

(60...70



2.2-

: 1-

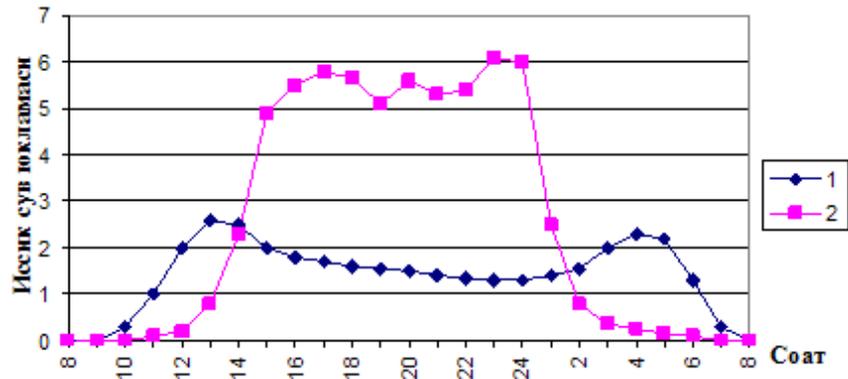
, 2-

1, 2

()

[20]

60...100



2.3-

1- ; 2-

(7...11

(17...24

9

15...16

5...6

1...2

f

Q

$$Q = G (t - t_0) C_n ; G = m G_1. \quad (2.30)$$

(2.20)

G

$t = 60 \text{ C}$

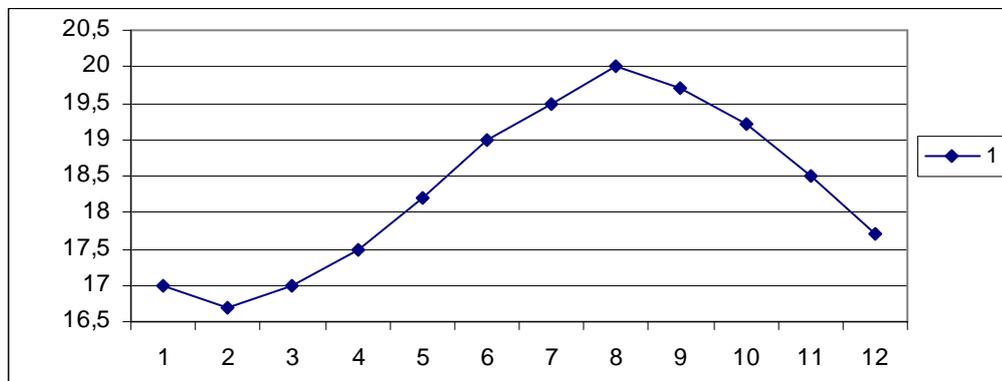
$$t = 17 \dots 20 \text{ C} \quad (2.4- \quad).$$

$$n=31 \text{ c} ; m=5; t =17 ; =1 / ; C=4190 /(\quad)$$

$$: G_{II} = 60 /(\quad) ,$$

$$Q_{I} = 5 \times 60 (60-17) 1 \times 4190 \times 31 = 1,676 \times 10^9 / = 1,676 \times 10^6 / ; G_{I2} = 100$$

$$/(\quad) , Q_{2} = 5 \times 100 (60-17) 1 \times 4190 \times 31 = 2,793 \times 10^9 / = 2,793 \times 10^6 / .$$



2.4-

t_{cc}

$$G = \frac{Q}{Q \eta} \quad (2.31)$$

$$G = G \quad (2.32)$$

$$Q = 38989 /^3 ; = 0,55 ; = 1,33.$$

$$G_I = \frac{1,676 \times 10^6}{38989 \times 0,55} = 78,12 \text{ }^3/ \quad (2.33)$$

$$G_I = 78,12 \times 1,33 = 103,9 \text{ } ./ \quad (2.34)$$

$$G_2 = \frac{2,793 \times 10^6}{38989 \times 0,55} = 130,2 \text{ } ^3/ \text{ } ; \quad (2.35)$$

$$G_2 = 130,2 \times 1,33 = 173,2 \text{ } . \text{ } ./ \text{ } . \quad (2.36)$$

Q G, G n, t (

).

$$Q_1 = 19,133 \times 10^6 \text{ } / \text{ } ; \quad Q_2 = 31,888 \times 10 \text{ } / \text{ } ;$$

$$: Q_1 = 898 \text{ } ^3/ \text{ } ; \quad Q_2 = 1485 \text{ } ^3/ \text{ } ;$$

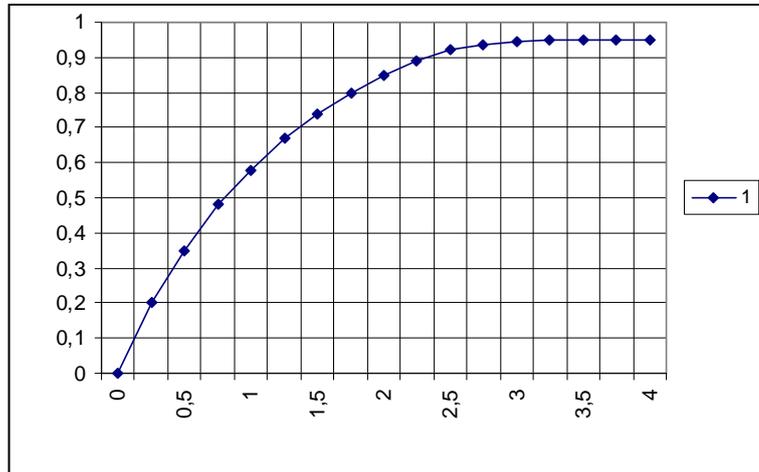
$$Q_1 = 1185 \text{ } . \text{ } ./ \text{ } ; \quad Q_2 = 1975 \text{ } . \text{ } ./ \text{ } .$$

:

$$Q = Q_{<} F \text{ } ; \quad Q_{<} = Q \quad (2.37)$$

f

$f=0,6$



2.5-

: 1 - f-

q-

q

$$q = Q_{<} F / Q = 1,1$$

$$(2.38)$$

$$F = 1,1 Q / Q_c = 1,1 \frac{Q}{Q} . \quad (2.39)$$

:

$$Q = 6516 \quad /(\text{ }^2 \text{ }) \\ = 1,23 \quad .$$

:

$$G_1 = 60 \quad /(\text{ }) ; Q_1 = 19,133 \times 10^6 \quad / \\ F_1 = 1,1 \frac{19133 \times 10^3}{6516 \times 10^3 \times 1,23} = 2,62 \quad ^2 = 2,7 \quad ^2 ;$$

$$G_2 = 100 \quad /(\text{ }) ; Q_2 = 31,888 \times 10^6 \quad / \\ F_2 = 1,1 \frac{31888 \times 10^3}{6516 \times 10^3 \times 1,23} = 4,38 \quad ^2 = 4,5 \quad ^2 .$$

...

$$= 0,4 \quad .$$

. Q

$$Q = 253,6 \quad /(\text{ }^2 \text{ }) , \quad = 1,7$$

$$Q_1 = 253,6 \times 1,7 \times 2,7 \times 0,4 = 465,6 \text{ M} \quad / \quad ;$$

$$Q_2 = 253,6 \times 1,7 \times 4,5 \times 0,4 = 776 \quad /o \quad ;$$

$$Q_1 = 1676 \quad /o \quad ; \quad Q_2 = 2793 \text{ M} \quad /o \quad .$$

$$f_1 = 465,6 / 1676 = 0,278 ; \quad f_2 = 776 / 2793 = 0,278 .$$

Q

f

f=1

q=3

2.6-

$$G_1 = 60 \text{ / () } : F_1 = 5^2;$$

$$f = 75,7 \%; G_2 = 100 \text{ / () } : F_2 = 9^2;$$

$$f = 81,4 \%$$

$$V = v F = 0,05 F ; \quad (2.40)$$

$$G_1 = 60 \text{ / () }, m = 5 : V = 0,25^3 = 250 ;$$

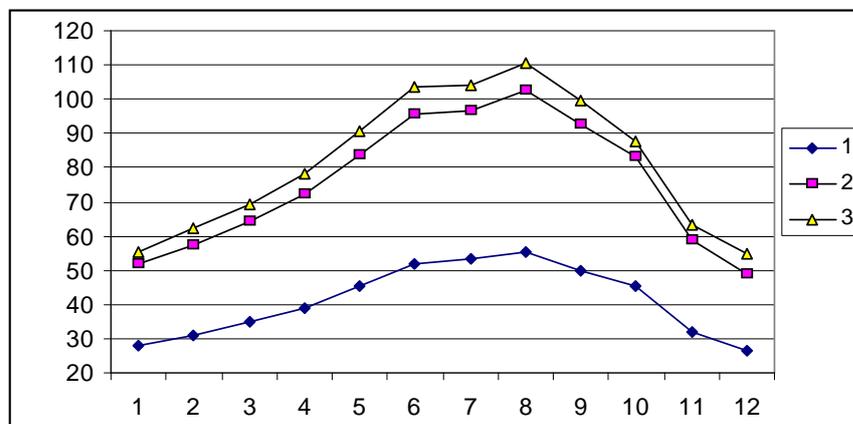
$$G_2 = 100 \text{ / () }, m = 5 : V = 0,45^3 = 450 .$$

$$Q_1 = 19,133 \times 10^6 \text{ / } ; Q_2 = 31,888 \times 10^6 \text{ / } .$$

$$G_{c1} = 898^3 / ; G_{c2} = 1485^3 / ;$$

$$G_{cl} = 1185 \text{ . / } ; G_{c2} = 1975 \text{ . / } .$$

:
 - 28...55%; - 52...100%
 898...
 1485^3 / 1185...1975 . / . [21]



2.6- . f , =5:

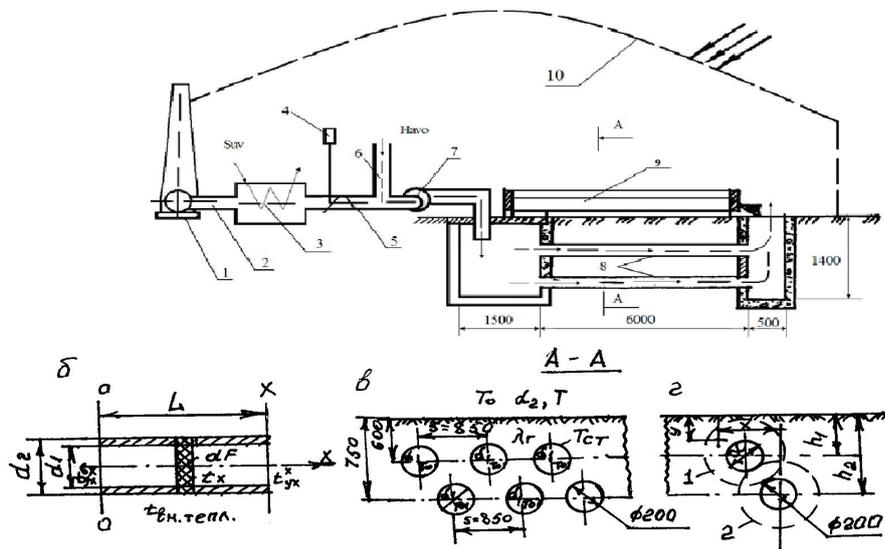
$$1 - G_1 = 60 \text{ / () }, F_1 = 2,7^2; G_2 = 100 \text{ / () }, F_2 = 4,5^2;$$

$$2 - G_1 = 60 \text{ / () }, F_1 = 5^2; 3 - G_2 = 100 \text{ / () }, F_2 = 9^2;$$

2.3.

[22]

2 0,3...0,5%
2



2.7-

(),

().

) 1- : 2- ; 3- ; 4-
; 5- ; 6- ; 7-
; 8- ; 9-
; 10- ;

) 1- ($d=200$), h_1, h_2

.

()

.

(1)

10-15%

.

, (2)-

(3)

(4)

(7)

(5)

(6)

2

0,3 ÷ 0,5 %

,

320

.

-

,

.

-

.

,

-

t

.

$$F = \frac{r}{t_{yx}} V_r \quad (23)$$

$$t_{yx} = (t_{yx} - t) \left(-\frac{KF}{V_r C_r} \right) + t \quad (2.41)$$

$$\delta = 3 \quad R_0 = 0,31 \frac{2 \cdot 0}{\dots} \quad (2.41)$$

$$t_{yx} = 45^0 C, \quad t = 17^0 C, \quad = 1,298 \frac{\dots}{\dots}, \quad t^x = 32,8^0 C$$

$$Re = \frac{V_r \cdot d_T}{V} \geq 2300 \quad (2.42)$$

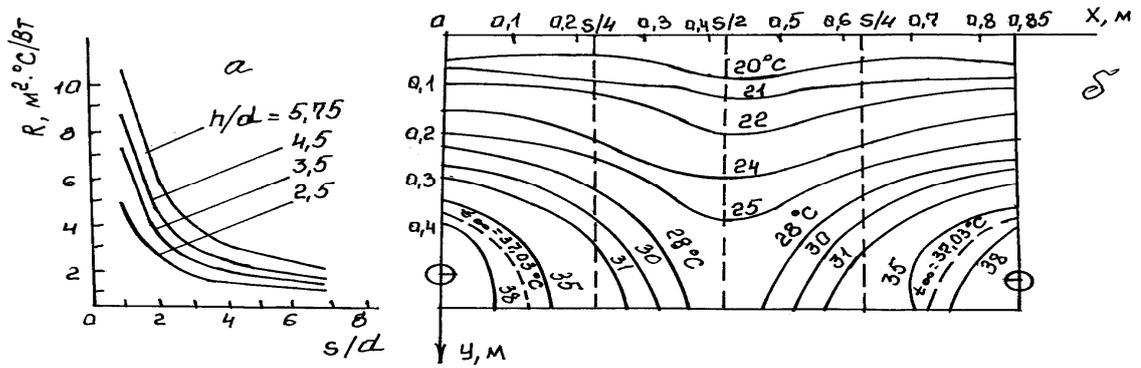
$$t_{r.n} = 25 \div 30^0 C, \quad \lambda = 2,6 \cdot 10^{-2} \frac{BT}{\dots}; \quad V = 16 \cdot 10^{-6} \frac{2}{c}$$

$$\alpha = 3,21 \frac{g^{0,8}}{d^{0,2}}; \quad (2.43)$$

$$\frac{S}{d} \quad \frac{h}{d}$$

$$R = \frac{1}{2\pi\lambda} \ln \left[\frac{2S}{\pi d} Sh \left(2\pi \frac{d}{S} \right) \right] \quad (2.44)$$

2.8-



2.8-

()

()

()

,

$$\left(\frac{h}{d}\right)$$

$$\left(\frac{S}{d}\right)$$

.

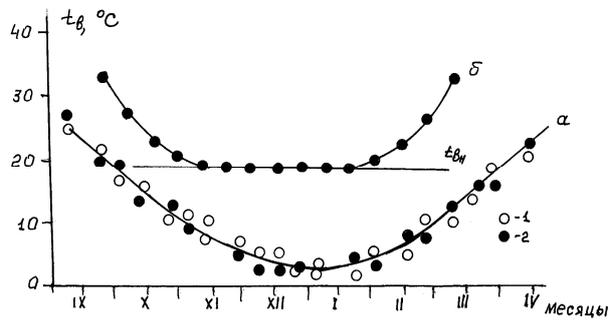
. (2.8- ,).

$$Q = 14,84 \frac{BT}{d}$$

.

,

. [24]



2.9- . 2014-2015 .(1) 2015-2016 .(2)

(), 2015-2016 .

(), t -

t .

2.9 ()- 2014-2015 .

,

2008-2009 .
 , 15-20% .
 2.9 ()- 2015-2016 .

t_B , $18,6^0$
 , 24^0
 16^0

() Δt G

, -
 () .
 t_{cp}
 t

505

, :

$$\Delta t = t_{cp} - t_B = \frac{(t_r + t_o)}{2} - t_B = \frac{(95 + 70)}{2} - 18 = 64,5^0 C. \quad (2.45)$$

$70-95^0$

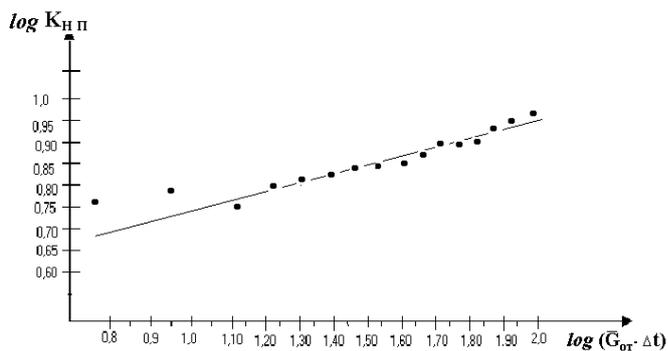
(K , / 0) -

:

$$K_{H.} = m \Delta t^n \cdot \bar{G}_{OTH}^P, \quad (2.46)$$

m, n, p-

; Δt -
, \bar{G}_{OTH} -



2.10-

$K_n \lg(\cdot \Delta \tau)$ lg

$$K_{H.} = 3,38 \cdot \Delta t^{0,2} \cdot \bar{G}_{OTH}^{0,066} \quad (2.47)$$

$$\bar{G}_{OTH} = 1 \quad \Delta t = 12 \div 82^0 C$$

w

G ,

2013

(,)

ö

1

2

100

XXI-

E,

$$3,86 \cdot 10^{26} \quad (3,86 \cdot 10^{33} \quad /)$$

$$1,57 \cdot 10^{18} \quad . /$$

10

(-) () -
 900 / ² , 6 850-
 5-15 / ,
 ,
 ,
 , -

55-65%
 , 30-32 . . / ²
 .
 1 . 10-13 ^{3/}
 . 700-800 / ²
 1200-1400 , 30-32⁰ ,
 50-55⁰ ,
 0,18-0,2 . . / .

1 4 / 560
 . . . / .
 , 6
 5 . ³ 6,4 . . .
 . ,
 30 % .

10-12%

()

:

25 %

55-75;

(/ ²),

50-70;

45-55.

75 %

6,33 / ²⁰ ,

3,4 / ²⁰ ,

5,1 / ²⁰ .

10

30-40%

[25].

60-80°

50%

59%

10%

200 ²

0,2÷0,3%,

10

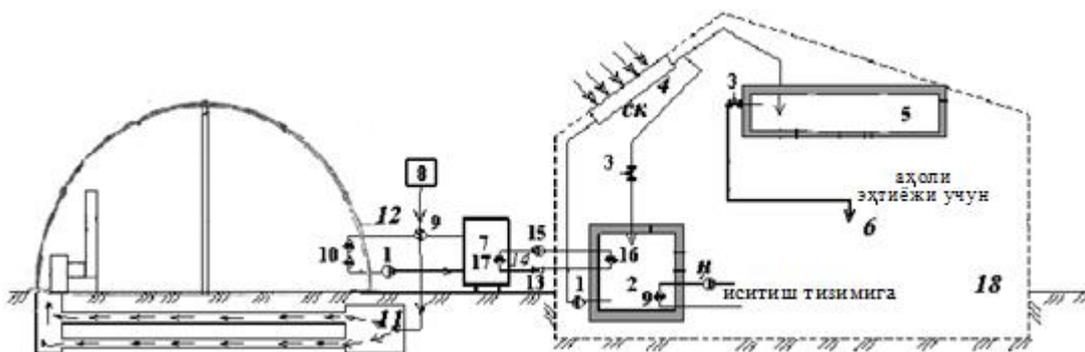
10÷12

, 10÷12 1³

45÷55%, . . . 25÷30 . . . /²

ö

ö



1- .

- 1- ; 2- ; 3-
- 4- ; 5-
- 6- ; 7-
- 8-
- 9- ; 10- ; 11-
- 12- ; 13-
- 14- ; 15-

; 16- ; 17-
; 18- .

12 18, () 14, 18
. 18, 14,
16 .

15 .
17 6 2,
+50 +60 ° .

1 2
, 8
+90 +100°
(10) . (8)

11 .
4 , 3 13

. 5²
, -
100²

.
() 0,2-0,4 % ,
10-20 1³
1 .

, ,
, , ,
, ,
, .

. [26]

200²

34 1²

30-40 %

100² , 5

III- .

3.1.

[27].

ó

$$\frac{dT_x}{dt} - K \frac{d^2T_x}{dt^2} - V_x \frac{dT_x}{dt} = 0 \quad (3.1)$$

T_x - ó

t ó

V_x -

(3.1)

$$\frac{dT_x}{dt} = K \frac{d^2T_x}{dt^2} + \frac{1}{v \cdot pv} \cdot \frac{dQ}{dt} \quad (3.2)$$

V-

(3.2)

$$T_t = T_{ak} \exp(-\beta \cdot t) \quad (3.3)$$

$$\beta_{\delta r} = \frac{K_{\delta r} F}{Cpv}$$

F ó

Q

$$\frac{dQ_u}{dt} = K \cdot F \cdot T \cdot \exp(-\beta \cdot t) \quad (3.4)$$

[28].

$$V_x \frac{dT_x}{dt} = \frac{dQ_u}{dt} \quad (3.5)$$

$$\frac{dQ_u}{dt} = \xi, \quad V_x / V_x \quad (3.6)$$

, ξ -
 m ó
 V_x -

$$V_x = \sqrt[3]{3} \quad (3.7)$$

, ó
 ó

$$V = h_x t \quad (3.8)$$

$$h_x = K_x Q_u |0,24 \gamma T_{ak} \quad (3.9)$$

ó
 Q_u ó
 ó
 γ ó
 ó

(3.4) ó(3.9)

$$\frac{dQ_u}{dt} = \frac{\xi_1 K Q_u - t T_{ak}}{0,24 \gamma \sqrt{3 K T m}} K \cdot F \cdot \exp(-\beta t) = T \quad (3.10)$$

$$\frac{dQ_u}{dt} = \frac{\xi_1 K Q_u t \cdot K \cdot F}{0,24 \gamma_0 \sqrt{3KT m}} \exp(-\beta t) = 1 \quad (3.11)$$

(3.11)

ó

$$T_x = \frac{\xi_1 K Q_u K F}{0,24 \gamma_0} \cdot \frac{1}{2} t^2 \exp(-2\beta t) = T_{ak} t^2 \exp(-2\beta t) \quad (3.12)$$

(3.12)

ó

V_x

V_x ,

$$Q_{ak} = mc_b T_{ak} = mc_x (T_2 - T_1) \quad (3.13)$$

$$Q_{ak} = mc_b T_{ak} = K_T T_{cx} T_{xak}^1 \quad (3.14)$$

$$K_T = \frac{Q_{ak}}{T_{xak}}$$

(3.11)ó(3.14)

$$T_{xak}(t) = K_T T_{xak} \int_0^t t^2 \exp(-2\beta t) dt = T_{ak} [1 - (1 - 2\beta^2 t^2) \exp(-2\beta t)] \quad (3.15)$$

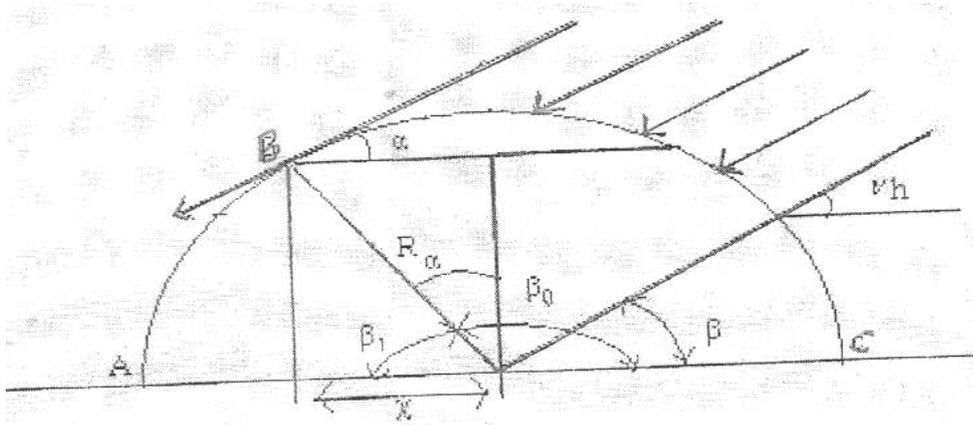
6-8 %

[29].

3.2.

$$100^2$$

[30]



3.1-

$$h = (90^\circ - \varphi) - \delta$$

$$\varphi = 39^\circ$$

$$\delta = 23,5^\circ; h = 28^\circ$$

$$\alpha = h = 28^\circ$$

$$\beta_0 = 90^\circ + \alpha = 118^\circ$$

$$\beta_1 = 180^\circ - 118^\circ = 62^\circ$$

$$Q = \perp \sin \alpha B n \quad (3.16)$$

$$\sin \alpha = \cos Z \sin \alpha = \sin \alpha \cdot \cos \delta \sin \tau \quad (3.17)$$

$$(\tau_{50}) = 0, \quad \varphi > \delta, a = \pi, \quad \varphi < \delta$$

$$\tau = 0$$

$$\alpha = \frac{\tau}{2} - (90 - \delta) \quad (3.18)$$

$$\varphi - \quad \oplus, \delta - \quad \ominus, \tau -$$

$$0-180^0$$

$$\tau < 90^0, \quad \oplus \quad ;$$

$$\tau > 90^0, \quad \ominus \quad ;$$

$$h = 0 - 180^0$$

$$h \quad \beta$$

$$\cos i = \sin \beta [\cos \delta (\sin \varphi \cos \alpha_n \cos \tau) - \sin \delta \cos \alpha_n] + \cos \beta [\cos \delta \cos \varphi \cos \tau - \sin \delta \sin \varphi] \quad (3.19)$$

$$\varphi - \quad \delta -$$

$\tau -$

$$i(\beta = 90^0)$$

$$\cos i = \cos \delta \cos \varphi \cos \tau - \sin \varphi \quad (3.20)$$

$$i(\beta = 90^0)$$

$$\cos i = \cos \delta (\sin \delta \cos \alpha_n \cos \tau - \sin \alpha_n \sin \tau) - \sin \delta \cos \varphi \cos \alpha_n \quad (3.21)$$

$$Q = Q_{\perp} \cos i Bn \quad (3.22)$$

[31].

$$Q = Q \quad (3.23)$$

: Q -

(/ ²)

$$R = \frac{Q}{Q} \quad (3.24)$$

$$\alpha = 50^\circ$$

()

()

30° 90°

$$\alpha = \pm 15^\circ$$

2%

$$\alpha = \pm 40^\circ$$

13%

$$k = \left(1 - \frac{Q}{Q}\right) kg + \frac{Q}{2Q} (1 + \cos \beta) + \rho \frac{(1 - \cos \beta)}{2} \quad (3.25)$$

ρ - , $\rho = -0,7$, $\rho = 0,2$;

Q - 1^2

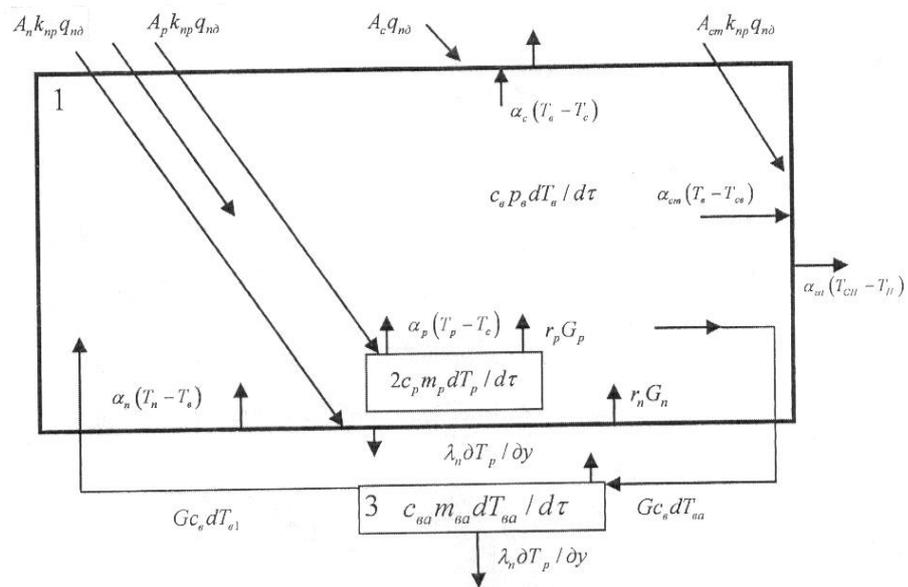
2500 / ² 6280 / ²

35-40%

[32].

3.3.

[33].



3.2-

1- , 2- , 3-

:

$$c \rho V \frac{dT}{d\tau} = Q_n + \alpha_n(T_n - T)F_n + \alpha_\rho(T_\rho - T) - \alpha_c(T - T_c) - \alpha_c(T - T_c) - Gc(T_0 - T_1) - Gc(T - T_H) \quad (3.26)$$

$$c \rho V \frac{dT}{d\tau} -$$

;

$$Q_n -$$

;

$$\alpha_n(T_n - T)F_n, \alpha_\rho(T_\rho - T) -$$

;

$$\alpha_c(T - T_c), \alpha_c(T - T_c) -$$

;

$$Gc(T_0 - T_1) -$$

;

$$Gc(T - T_H) -$$

.

:

$$c_c m_c \frac{dT_c}{d\tau} = A_c q_{nd} F_c + \alpha_c(T_\varepsilon - T_c)F_c + \alpha_n(T_c - T_n)F_c + rG_{kd} c F_c; \quad (3.27)$$

$$c m_c \frac{dT_c}{d\tau} -$$

;

$$A_c q_{nd} F -$$

.

$$\alpha_c(T - T)F_c, \alpha(T - T)F -$$

;

$$rG_{kd} c F -$$

;

:

$$c_{cm} m_{cm} \frac{dT_{cm}}{d\tau} = A_{cm} \kappa_{\gamma\beta} q_{nd} F_{cm} + \alpha_{cm}(T_\varepsilon - T_{c\varepsilon})F_{cm} + \alpha_{ncm}(T_{cn} - T_n)F_{cm}; \quad (3.28)$$

$$c_p m_c \frac{dT_c}{d\tau} -$$

;

$$A_c \kappa_n q_n F_c - \quad ;$$

$$\alpha_c (T_c - T_\varepsilon) F_c, \alpha_c (T_c - T_\varepsilon) F_c -$$

$$- \quad ;$$

, :

$$\frac{dT_n}{d\tau} = \alpha_n \frac{d^2 T_n}{dy^2} \quad (3.29)$$

$$: = 0 \quad :$$

$$\lambda_n \frac{dT_n}{dy} F_n = A_n \kappa_{np} q_{n\delta} F_n + \alpha_n (T_n - T_\varepsilon) F_n - r G_n F_n \quad (3.30)$$

$$y = \delta, \quad t_n = t = const \quad ; \quad \lambda_n \frac{dT_n}{dy} F_n -$$

;

$$A_n \kappa_n q_n F_n - \quad ;$$

$$\alpha_n (T_n - T_\varepsilon) F_n - \quad ;$$

$$r G_n F_n - \quad ;$$

$$c_p m_p \frac{dT_p}{d\tau} = A_p \kappa_p q_p F_p + \alpha_p (T_p - T_\varepsilon) F_p - r G_p F_p \quad (3.31)$$

$$\frac{dT}{d\tau} -$$

$$; A_n \kappa_n q_n F_n - \quad ; \alpha (T - T_\varepsilon) F -$$

$$; r G F -$$

;

:

$$c_{sd} m_{sa} \frac{dT_{sa}}{d\tau} = w_m \rho_s c_s \frac{\pi D_m^2}{4} L_m (T_{s0} - T_{s1}) n_m \quad (3.32)$$

$\alpha_c, \alpha_n, \alpha_p, \alpha_{cm}, \alpha_c$

,

$$\alpha_i = \alpha_{ki} + \alpha_{ui} \quad (3.33)$$

(3.26) (3.32)

. [34]

()

)

$$Q = \frac{Q \cdot}{29330 \cdot 10^6}, \quad \dots / ; \quad (3.34)$$

, Q -

, /³ /

)

$$Q = \frac{i_1 \cdot}{4,187 \cdot 10^9}, \quad / , \quad (3.35)$$

, -

, /

³/ ;

$i_1 \cdot t_1$

, /

/³.

$$Q = \frac{(i_1 - i_2) \cdot \beta \cdot l \cdot 10^{-9}}{4,187}, \quad / \quad (3.36)$$

, i_1 -
 , / ;
 i_2 - , / ;
 - ;
 l - ;
 , $l=0,8-0,9$;
 - () , / $^3/$.
 :

$$\beta = \frac{T \cdot}{\cdot \alpha}, \quad (3.37)$$

, \cdot - , / ;
 \cdot - () , / .
 ,

[35]

$$\Delta\beta = \beta \cdot Q \cdot \delta, \quad (3.38)$$

, -
 $\cdot \cdot /$; Q -
 , / ; -

$$\begin{aligned}
 & \left(\dots, \dots, \dots \right) \\
 & = 760 \dots \dots \dots t_a = 0^0 \\
 & \dots \dots \dots : \\
 & q = m(C_1 t_1 - C_2 t_2) = m \Delta i; \left(\dots / \dots / ^3, \dots / \dots \right) \quad (3.39) \\
 & m- \dots \dots \dots , \\
 & (\dots^3) / \dots ; i- \dots \dots \dots / \dots ; t_1- \\
 & \dots \dots \dots ; ^0 ; 1- \dots \dots \dots , \dots / \\
 & ^0 ; t_2; 2- \dots \dots \dots , (\dots / ^0).
 \end{aligned}$$

$$\begin{aligned}
 & \dots \\
 & : \\
 & Q = Q \cdot \eta; \quad (\dots) \quad (3.40)
 \end{aligned}$$

, - \dots \dots \dots

$$\begin{aligned}
 & \dots \\
 & : \\
 & Q_x = Q_T \cdot E; \quad (\dots) \quad (3.41)
 \end{aligned}$$

, - \dots \dots \dots

$$\begin{aligned}
 & \dots \\
 & : \\
 & B = {}_3 Q_n = Q_T {}_3 \sigma, \dots \dots \quad (3.42)
 \end{aligned}$$

, Q_n- \dots \dots \dots , (\dots);

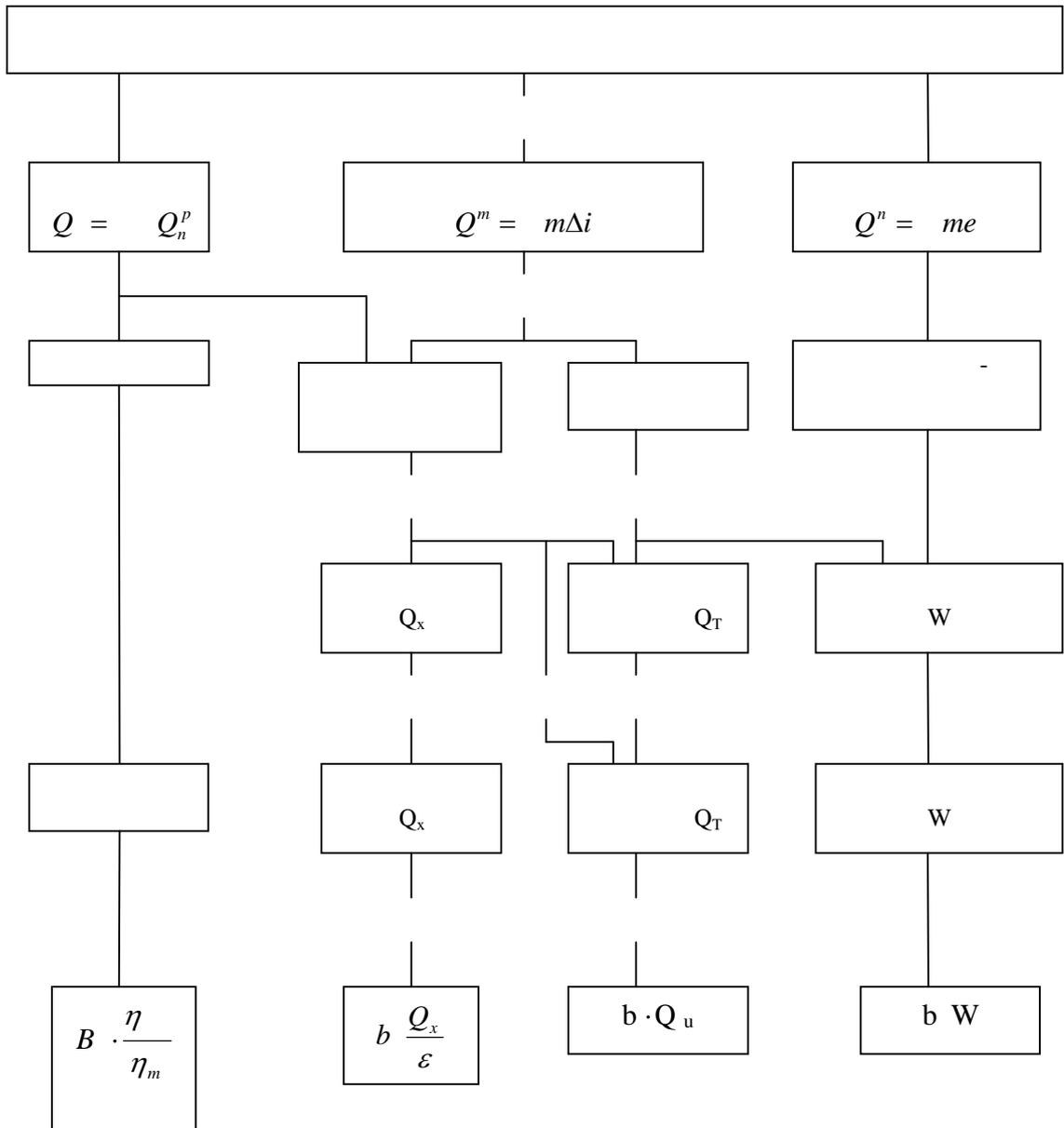
Q_T- (\dots); -
; 3-

$$\begin{aligned}
 & \dots \dots \dots / \dots \dots \dots , \dots \dots \dots , \\
 & {}_3 = \frac{0,143}{\eta_3}, \dots \dots \dots / \dots \dots \dots ; \quad {}_3 = \frac{0,342}{\eta_3}, \dots \dots \dots / \dots \dots \dots ;
 \end{aligned}$$

3-

\dots \dots \dots

3.1.-



16÷20%

[36]

1)
 $120 \div 140^0$;

2) $\dots = 1,12$;

3) \dots
 $= 92\%$;

4) $\dots \text{ é } 6400 \text{ }^3/$;

5) $\dots \text{ ót } t=18^0$.

\dots
 $\dots = 91,766\%$; $\dots = 4,805\%$; $\dots = 1,715\%$; $\dots = 0,963\%$;
 $\dots = 0,288\%$; $N_2 = 0,102\%$; $CO_2 = 0,361\%$.

$V_0 = \frac{3}{3} - 1^3$;

$V_{N_2} = 8,19 \frac{3}{3}$; $V_{RO_2} = 1,12 \frac{3}{3}$; $V_{H_2O} = 2,28 \frac{3}{3}$.

$\dots : \rho = 0,76 \frac{3}{3}$

() :

$\dots = 1,0$ $V = 9,31 \frac{3}{3}$.

$V_H = [V_c + V_{H_2O} + V_0(\alpha - 1)] = 6400[9,31 + 2,28 + 10,35(1,5 - 1)] = 81450 \frac{H^3}{3}$

$V_{\rho H} = V_H \cdot 0,5 = 40725 \frac{H^3}{3}$.

$$V_{iH} = V_{\rho H} \cdot \frac{t_1 + 273}{273} = 52000 \frac{3}{\dots}$$

$$2 = \frac{0,13 + X \cdot \alpha}{\alpha - 0,058} = 0,133 \frac{\dots}{\dots};$$

$$2 = \frac{0,0006382 + 0,004 \cdot \alpha}{0,199 + \alpha} \cdot 2,7183^{0,062 \cdot t_2} = 0,063 \frac{\dots}{\dots};$$

$$Q_k = V_{\rho H} [t_1 - t_2] + 435 \frac{0,133 - 0,063}{0,6 + 0,133} = 2112828,8 \frac{\dots}{\dots} = 2,45$$

2,45

1

$$\frac{2112828,8}{7000} = 301 \quad 1 \quad 301 \cdot 24 = 7224$$

3.4.

()

()

$$\begin{aligned}
 & \cdot \\
 & : \\
 & = + \cdot ; \tag{3.43} \\
 & , - \quad , / ; \\
 & - \quad , / ; \\
 & - \quad , \\
 & =0,12 \quad . \\
 & - \quad , /
 \end{aligned}$$

$$\begin{aligned}
 & , \\
 &) \\
 & : \\
 & = + \cdot ; \tag{3.44}
 \end{aligned}$$

$$\begin{aligned}
 &) \\
 & = + \cdot ; \tag{3.45} \\
 & ,
 \end{aligned}$$

$$\begin{aligned}
 & : \\
 & = - = - - (-); \tag{3.46} \\
 & >0
 \end{aligned}$$

() (),

- ;

- - ;

- ;

- ,

,

;

- ;

- ,

.

.

. [40]

- 1) . . . ;
- 2) ;
- 3) . . . ;
- 4) ;
- 5) ;
- 6) - . . .

- 1) (/ , ^{3/} . / , ^{3/});
- 2) (, , ,);
- 3) ;

Q

4)

(, , , ...).



3.3.-

$$= 0,143 \left(\frac{\alpha}{q} \right) \cdot 1,16; \quad (3.47)$$

-

$$q^{-1} \quad 1^3$$

$$200^2$$

$$G=7,24$$

$$G=1400000$$

$$200^2$$

$$\varepsilon_T = 4,03$$

$$4,1$$

1.

-

2.

-

3.

-

$$t_x = t_0 + (t_1 + t_2) \cdot C^{\rho \cdot v d^2}$$

$$t_{yx}^x = (t_{yx} - t_{BH.}) \left(-\frac{KF}{V_r \cdot C_r} \right) + t_{HB.}$$

4.

,

B_i -

$$d \cong 200$$

5.

$$10 \div 20$$

$$1^3$$

2

$$0,2 \div 0,4 \%$$

$$250 \div 300 \quad / \quad ^2 \quad \quad \quad 1 \quad ^3$$

$$14,67 \frac{BT}{3} \quad ,$$

$$200 \quad ^2 \quad 3 = 600 \quad ^3 \quad \quad \quad 8,8$$

$$, \quad 0,776 \quad .$$

7.

$$- \quad ,$$

$$14,84 \quad / \quad .$$

$$(d = 200 \quad) \quad \quad \quad V = 0,08 \div 0,4 \quad /$$

$$, \quad \quad \quad Re = 10^3 \div 0,5 \cdot 10^4$$

8.

-

$$, \quad \quad \quad 11 \div 15\% \quad \quad \quad , \quad 30\%$$

$$0,61 \quad ^2 / \quad ^3$$

$$(\quad) \quad , \quad 122 \quad ^3 \quad .$$

$$9. \quad \quad \quad 200 \quad ^2$$

$$G=7,24$$

$$G=360000$$

$$. \quad 200 \quad ^2$$

$$\varepsilon_T = 4,03$$

10. , 4,1 .

.
40-45%

-

1²

30 ÷ 32

.

1. . . ., «
- » , « »
, 2013 2 - .
2. «
» ∴
. 1997 ., 11-12 , 295- .
3. « » .
. 1997 ., 9-
, 225- .
4. 2015 9- 98- , 43- , 549-
õ õ .
5. . . õ
õ, . , ,
1967 .
6. . ., . õ -
-
õ,
-
, , 1972 .
7. . , . . õ
ö. , . 1977 .
8. . . . õ õ .
« ». 1995 .
9. . . õ -
ö// , , . ó :
, 2008. - . 174-177.

10. . . , . . , ð
 ö// - . 2012
11. . . , ð
 ö// -
 . 2012
12. . . ð
 -
 ö . , , 1970.
13. . .
 , . .
 , 1973 .
14. . . , . . ð ö ,
 ð ö, 1972 .
15. . . ð
 ö . . , , 1972.
16. . ð
 - ö . ,
 , 1974 .
17. . . ð ,
 -
 - ö
 . . , , 1967 .
18. . . ð
 - : ö. - :: , 1990 .
19. . , . . ð
 ö. , . 1988 . 282.
20. . , . . ð
 ö , . 1983 . 84.
21. . . « » 1976 .

22. . . , . . . ð
 ö. . , . 1977 . 420.
23. . . . ð
 ö . . . 1999 . 208.
24. . . . ð XXI
 II ö. , .
 2005 . 5-6. 27-42.
25. . . .
 : , 1989 .
26. . . , . . .
 . ó . . . , 1988 .
27. . . . ð
 - ö . . - . 1988 .
28. . , ð
 ó ö 1985 . 43-70.
29. . , ð
 , ö
 . // . 2010 . 2. 19-24.
30. ð ()ö.
 ó , 1993
31. . . , . . . , ð
 ö. ó , 1996
32. . . , . . , ð
 ö, ó . « » , 1980.
33. . . , ð ö.
 : . 2000
34. Srolding D.B., Ratankar S.V. ðHeat and mass Transfer in boundary
 laersö. London. Edward Arnolds, 1989
35. Truesdell C. ðRational thermodynamicsö. N.Y. Mc.Graw.Hili. 1992

46.
ó ó
2015 .45-48 .

47.
3 2015, 16-19 .

48.
ó ó
2016 .45-48 .

:

- [www.ziyonet.uz.](http://www.ziyonet.uz) ó
- www.energy.com
- <http://rbip.bookchamber.ru>
- <http://energy-mgn.nm.ru>
- <http://www.WSP.ru>
- [http://www.rosteplo.ru:](http://www.rosteplo.ru)
- <http://www.abok.ru>
- <http://www.03-ts.ru>